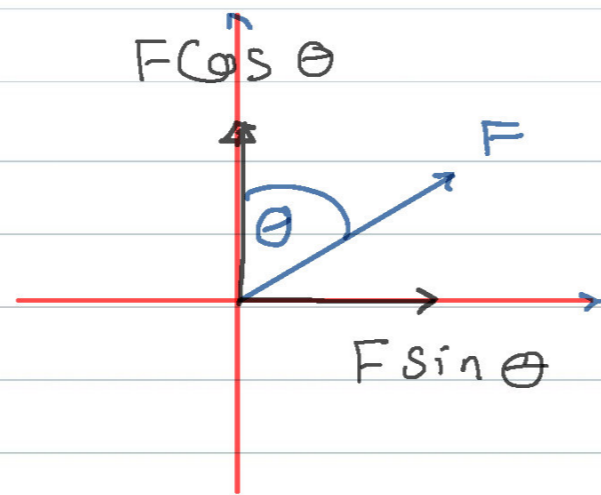


Introduction – Concept of Stress

Rectangular/Cartesian Components Method

$$\vec{F} = (F_x) \hat{i} + (F_y) \hat{j}$$

$$F = \sqrt{F_x^2 + F_y^2}$$



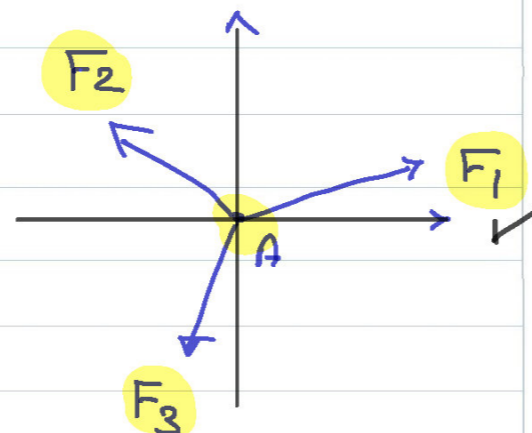
Equilibrium of a Particle

@ rest

1) Resolve

$$\sum F_x = 0 \quad \rightarrow +$$

$$\sum F_y = 0 \quad \uparrow +$$



Moment of the force

(vector)

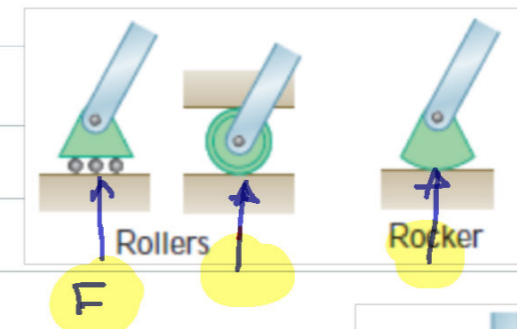
$$M = \begin{matrix} \epsilon r \times d_{\perp} \\ x \quad y \\ y \quad x \end{matrix} \left. \begin{matrix} \text{ccw} \quad \curvearrowleft \quad + \\ \text{cw} \quad \curvearrowright \quad - \end{matrix} \right\}$$

Equilibrium of Rigid Bodies

$$\sum F_x = 0 \quad \rightarrow + \quad \sum F_y = 0 \quad \uparrow + \quad \sum M = 0 \quad \curvearrowright +$$

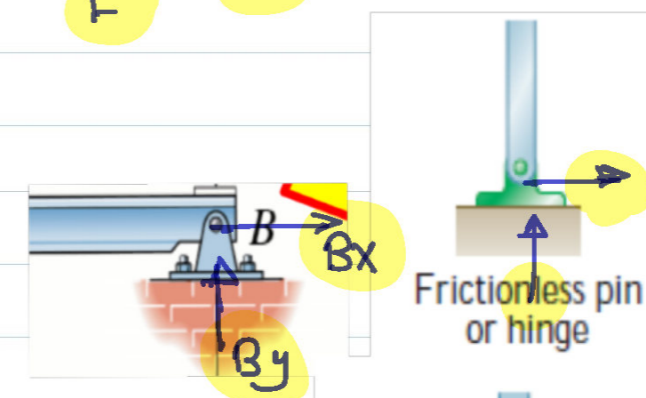
Supports Reactions :-

1) Roller



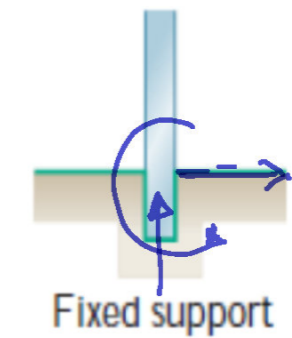
1- Reaction

2) Pin



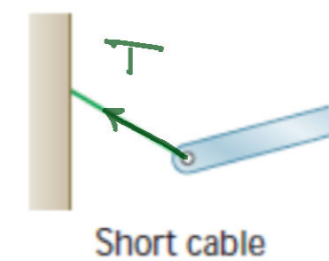
2- Reaction

3) Fixed



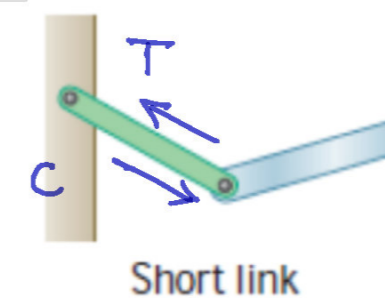
3- Reaction

4) Cable



only tension

5) Link



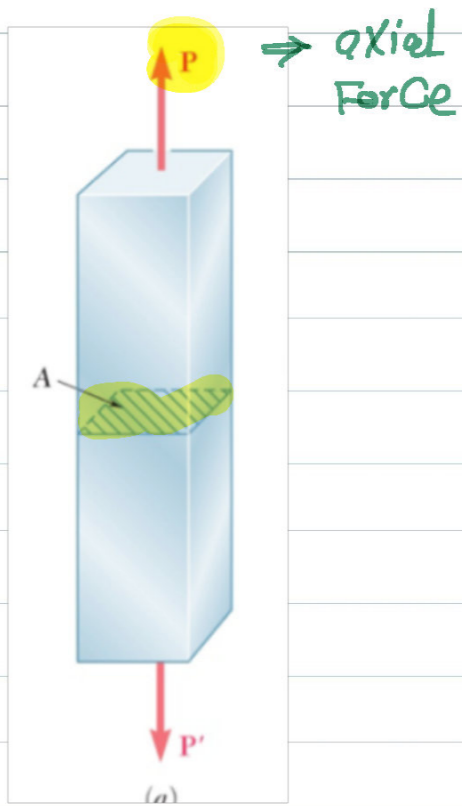
tension
or
compression

Concept of Stress

$$\text{Stress} = \frac{\text{Force}}{\text{Area}} \left[\frac{\text{N}}{\text{m}^2} = \text{Pa} \right]$$

Normal stress

$$P \perp A$$

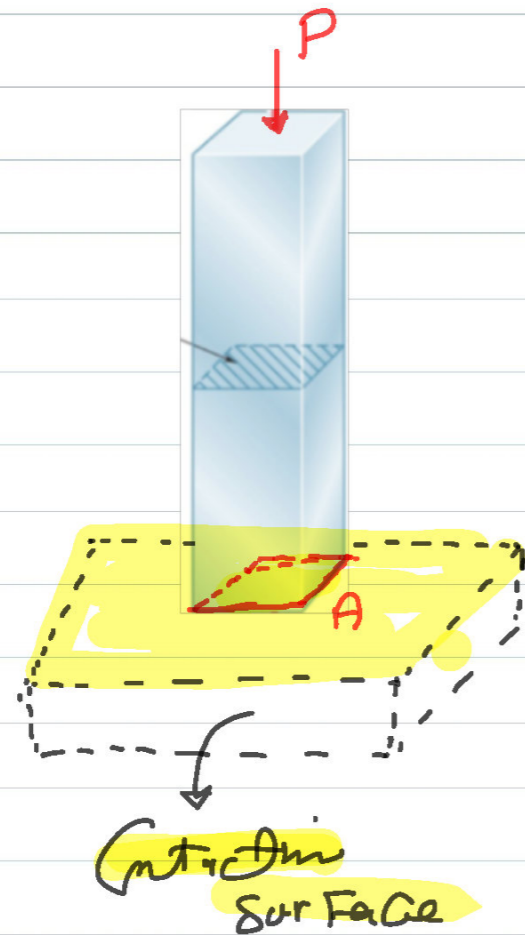


$$\sigma_{av} = \frac{P}{A}$$

⊕ Tension Force
⊖ Compression Force

Bearing stress

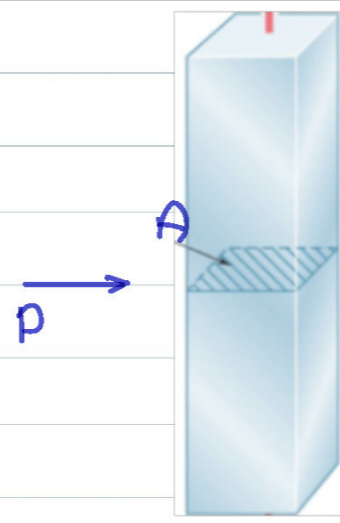
$$P \perp A$$



$$\sigma_b = \frac{P}{A}$$

Shear stress

$$P \parallel A$$



$$\tau_{av} = \frac{P}{A}$$

Single Shear Double Shear

Shearing Stress Examples

Single Shear

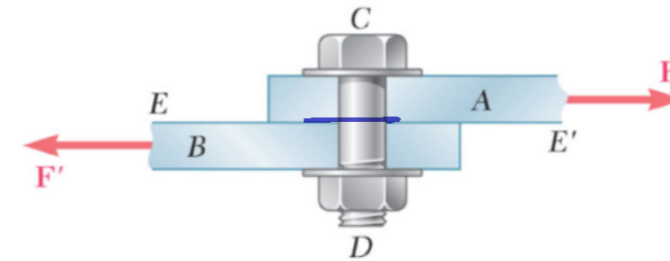
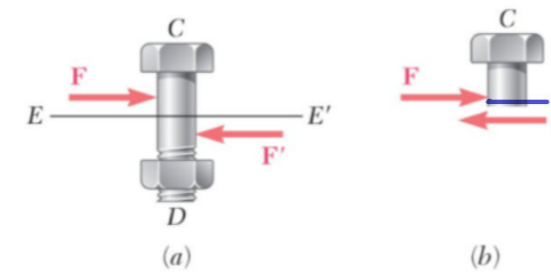


Fig. 1.16 Bolt subject to single shear.



2-Members
1-Cut

$$\tau_{av} = \frac{F}{A_{\text{bolt}}}$$



Double Shear

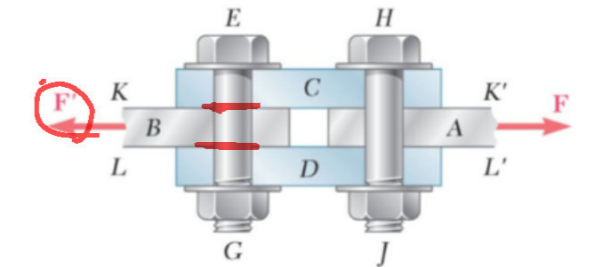
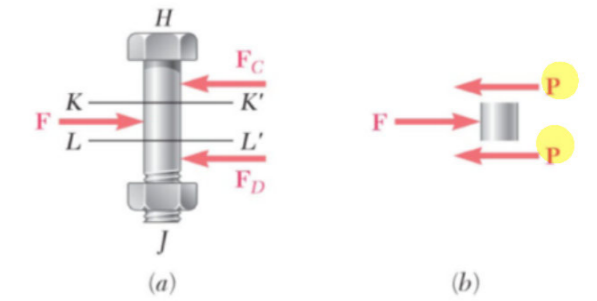
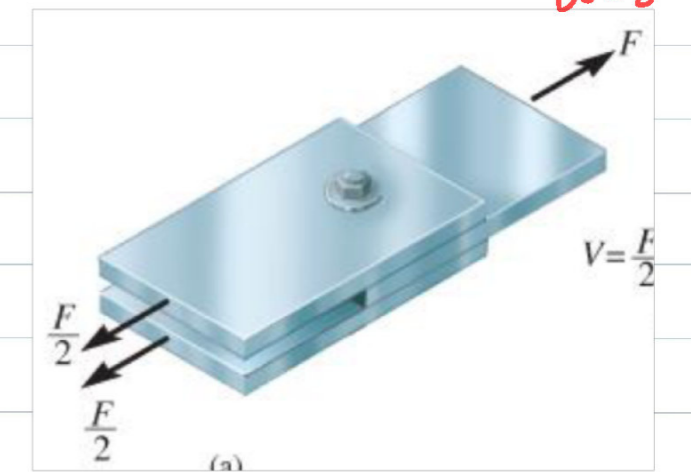


Fig. 1.18 Bolt subject to double shear.



3-Members
2-Cuts

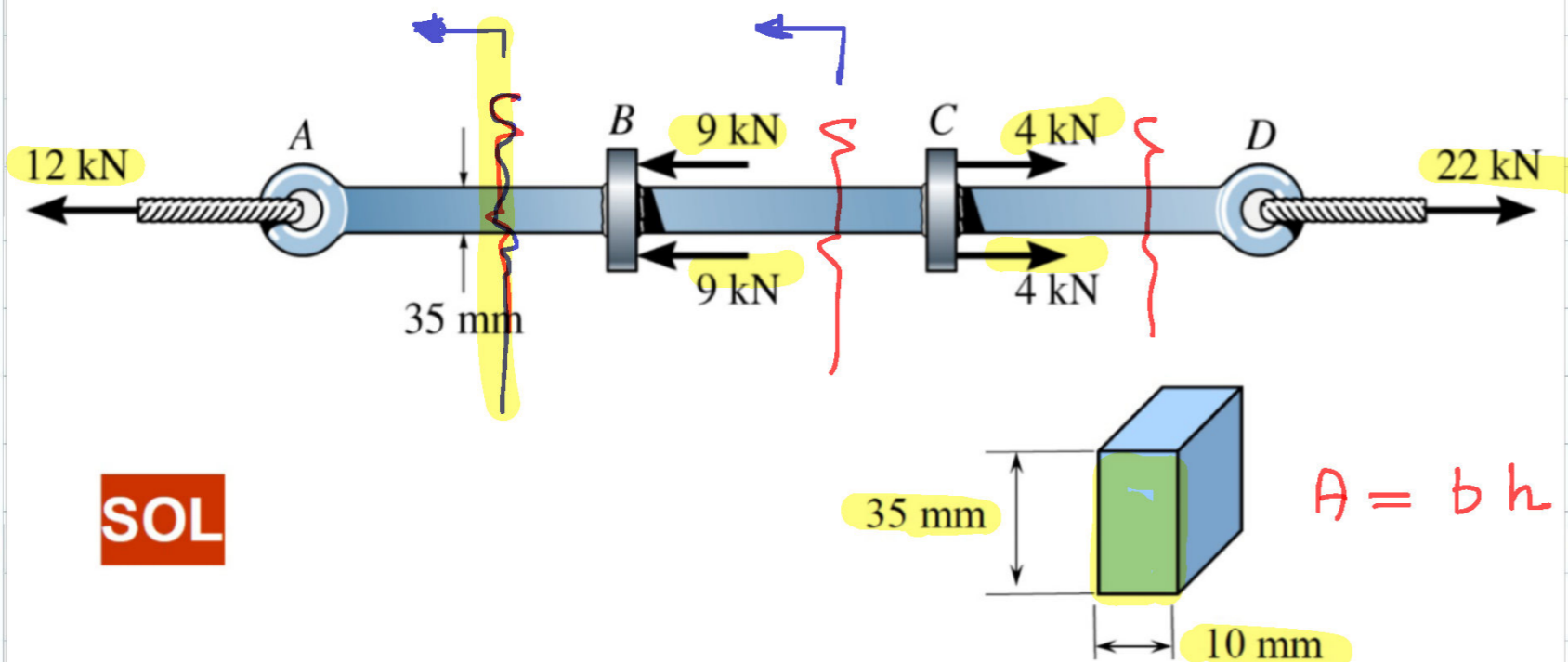
$$\tau_{av} = \frac{F}{2 A_{\text{bolt}}}$$



EXAMPLE 1.6

Bar width = 35 mm, thickness = 10 mm

Determine max. average normal stress in bar when subjected to loading shown.

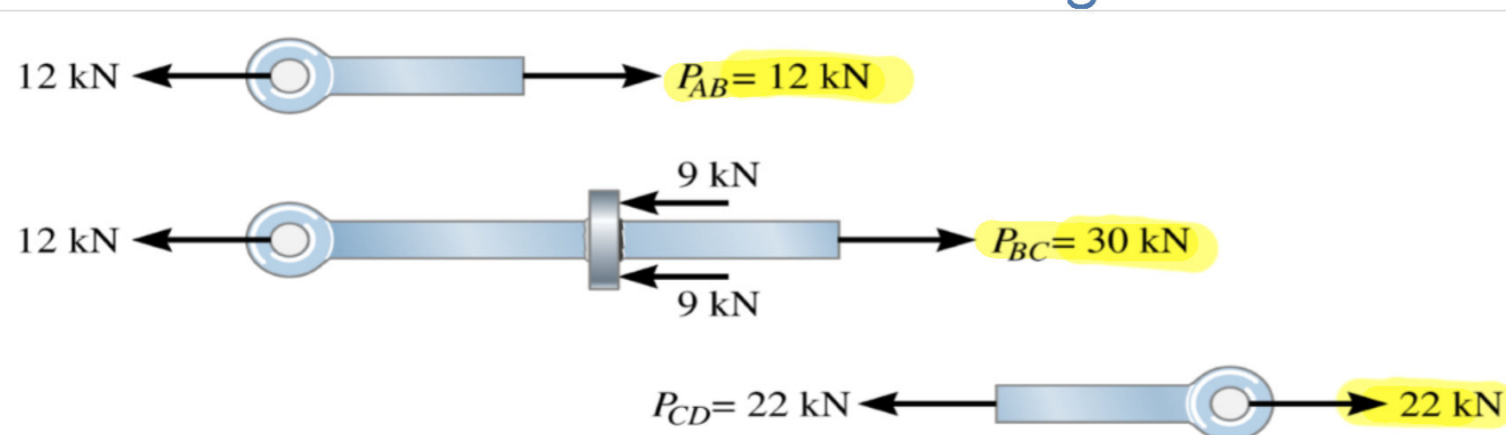


SOL

Area is constant

$$\sigma_{Max} = \frac{P_{Max}}{A}$$

Section \rightarrow change force
 \rightarrow change area



$$P_{AB} = 12 \text{ kN (tension)}$$

$$P_{BC} = 12 + 9 + 9 = 30 \text{ kN (tension)} \checkmark$$

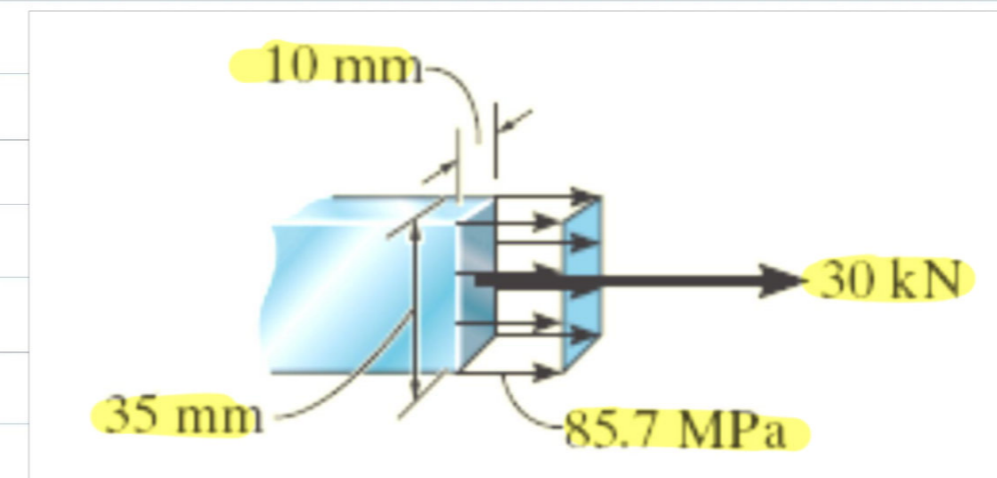
$$P_{CD} = 22 \text{ kN (tension)}$$

$$\sigma_{Max} = \frac{P_{Max}}{A} = \frac{P_{BC}}{A}$$

$$= \frac{30 \times 10^3}{0.035 \times 0.01}$$

$$= 85.7 \text{ MPa}$$

tensile stress



Challenging Problem P1.1

A stainless steel tube with an outside diameter of 60 mm and a wall thickness of 5 mm is used as a compression member. If the normal stress in the member must be limited to 200 MPa, determine the maximum load P that the member can support.



CORRECT ANSWER

$$P_{max} = 172.8 \text{ kN}$$

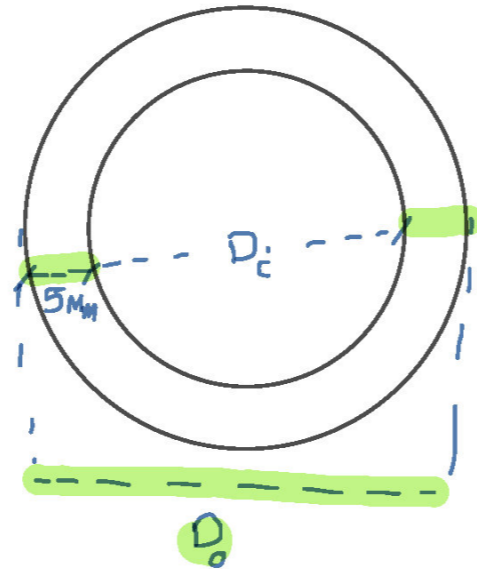
$$D_o = 60 \text{ mm}$$

$$D_i = 60 - 2(5) = 50 \text{ mm}$$

$$\begin{aligned} A &= \frac{\pi}{4} (D_o^2 - D_i^2) \\ &= \frac{\pi}{4} \left(\left(\frac{60}{1000}\right)^2 - \left(\frac{50}{1000}\right)^2 \right) \\ &= 8.64 \times 10^{-4} \text{ m}^2 \end{aligned}$$

$$\sigma_{max} = \frac{P_{max}}{A} \Rightarrow P_{max} = \sigma_{max} A$$

$$\begin{aligned} P_{max} &= 200 \times 10^6 \times 8.64 \times 10^{-4} \\ &= 172.8 \text{ kN} \end{aligned}$$



37

$$A_{net} = \pi R^2 = \frac{\pi D^2}{4}$$

Challenging Problem P1.2

A 2024-T4 aluminum tube with an outside diameter of 90 mm will be used to support a 285 kN load. If the normal stress in the member must be limited to 165 MPa, determine the wall thickness required for the tube.

CORRECT ANSWER

$$t_{min} = 6.59 \text{ mm}$$

$$\sigma_{max} = \frac{P}{A} \Rightarrow A = \frac{P}{\sigma_{max}} = \frac{285 \times 10^3}{165 \times 10^6}$$

$$A = 1.73 \times 10^{-3} \text{ m}^2$$

$$A = \pi (R_o^2 - R_i^2)$$

$$1.73 \times 10^{-3} = \pi \left[\left(\frac{45}{1000}\right)^2 - R_i^2 \right]$$

$$R_i = 38.4 \text{ mm}$$

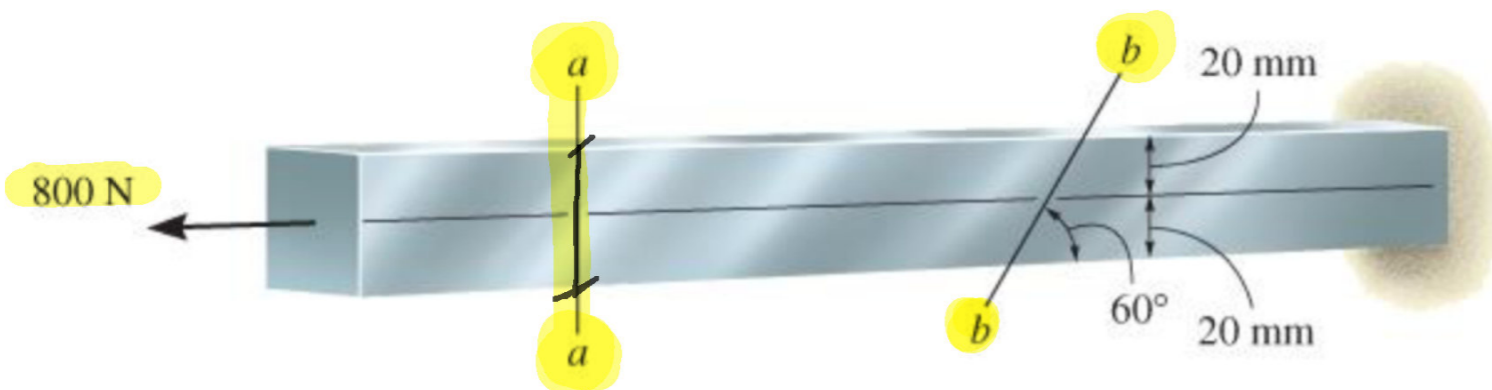
$$\begin{aligned} t &= R_o - R_i = 45 - 38.4 \\ &= 6.59 \text{ mm} \end{aligned}$$

EXAMPLE 1.10

Determine:

- average **normal stress**
- average **shear stress**

acting along section planes **a-a**, and section plane **b-b**.



Depth and thickness = 40 mm x 40 mm

cut a-a :-



$$P = 800 \text{ N [axial force]}$$

$$\sigma_{av} = \frac{P}{A} = \frac{800}{0.04 \times 0.04} = 500 \text{ kPa}$$

tensile stress (+)

No shear force @ section a-a

$$\tau_{avg} = 0$$

cut b-b :-

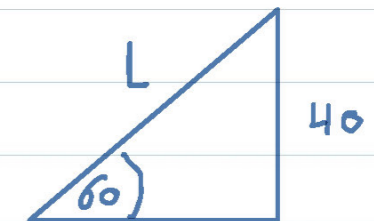


$$N = 800 \cos 30 = 692.8 \text{ N}$$

$$V = 800 \sin 30 = 400 \text{ N}$$

$$\sin 60 = \frac{40}{L}$$

$$L = \frac{40}{\sin 60}$$



$$\sigma_{av} = \frac{N}{A} = \frac{692.8}{0.04 \times 0.04 / \sin 60} = 357 \text{ kPa}$$

$$\tau_{av} = \frac{V}{A} = \frac{400}{0.04 \times 0.04 / \sin 60} = 217 \text{ kPa}$$

Factor of Safety

$$F.S = \frac{\sigma_{ult}}{\sigma_{all}} \quad \sigma_{ult} \Rightarrow \text{Fail}$$

$\sigma_{all} \Rightarrow$ allowable stress \Rightarrow Usef for design

$$A = \frac{P}{\sigma_{all}}$$

$$F.S = \frac{F_{ult} \Rightarrow F_{fail}}{F_{all}}$$

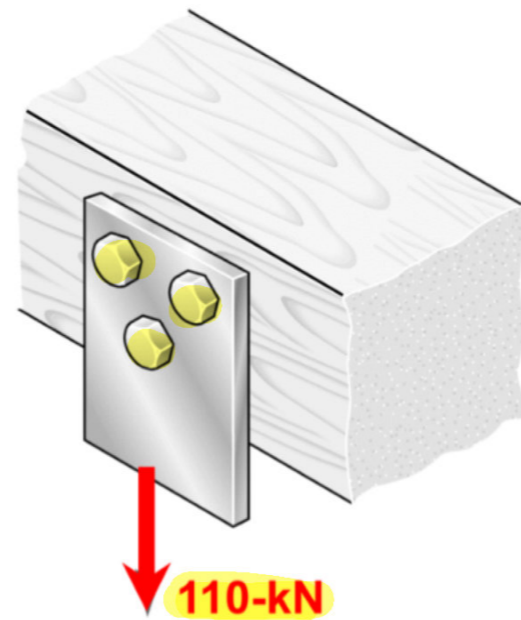
$$F.S = \frac{\tau_{ult} \Rightarrow \tau_{fail}}{\tau_{all}}$$

$$F.S > 1$$

$$\tau_{ult} = \frac{P_{ult}}{A}$$

PROBLEM 1.45

Three **18-mm-diameter** steel bolts are to be used to attach the steel plate shown to a wooden beam. Knowing that the plate will support a **110-kN** load and that the **ultimate shearing stress** for the steel used is **360 MPa**, determine **the factor of safety for this design**.

CORRECT
ANSWER

$$FS = 2.50$$

$$P = 110 \text{ kN}$$

$$\tau_{ult} = 360 \text{ MPa}$$

For one bolt

For each bolt

$$A = \frac{\pi d^2}{4} = \frac{\pi}{4} \left(\frac{18}{1000} \right)^2 = 254.47 \times 10^{-6} \text{ m}^2$$

$$P_u = A \tau_{ult} = 254.47 \times 10^{-6} \times 360 \times 10^6 = 91.61 \times 10^3 \text{ N}$$

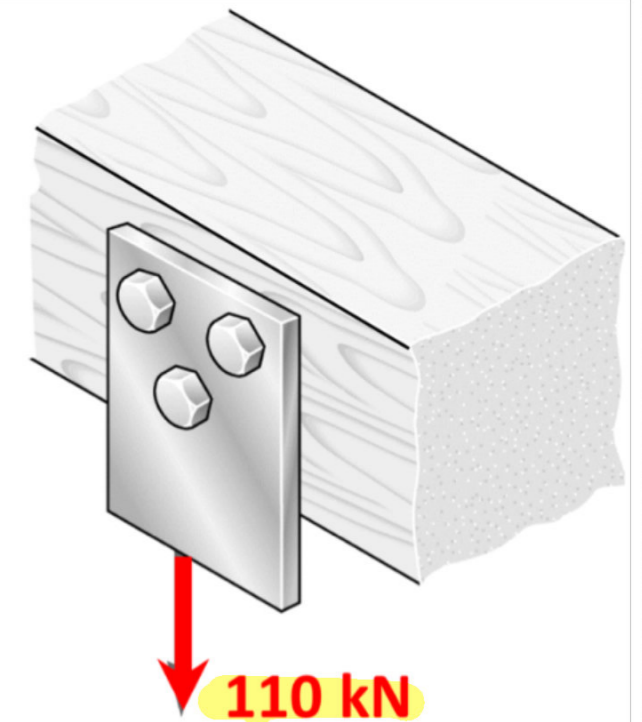
For the three bolts:—

$$P_u = 3 \times 91.61 \times 10^3 = 274.83 \times 10^3 \text{ N}$$

$$F \cdot S = \frac{P_{ult}}{P} = \frac{274.83 \times 10^3}{110 \times 10^3} = 2.5$$

PROBLEM 1.46

Three steel bolts are to be used to attach the steel plate shown to a wooden beam. Knowing that the plate will support a **110-kN** load, that the ultimate shearing stress for the steel used is **360 MPa**, and that a factor of safety of **3.35** is desired, determine the **required diameter of the bolts**.

CORRECT
ANSWER

$$d = 20.8 \text{ mm}$$

$$F \cdot S = 3.35$$

$$\tau_u = 360 \text{ MPa}$$

For one bolt

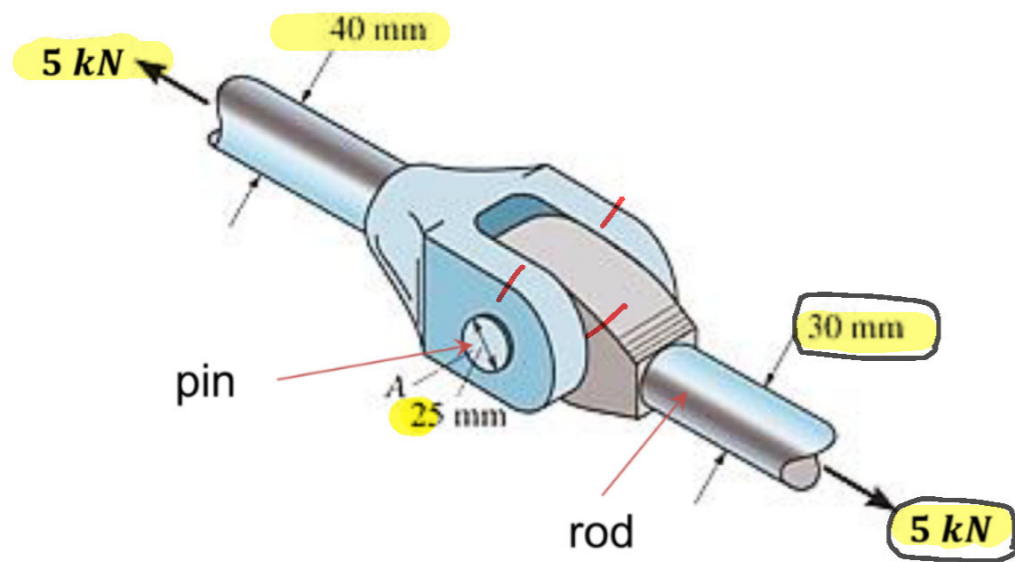
For each bolt:—

$$P = \frac{110}{3} = 36.667 \text{ kN}$$

$$F \cdot S = \frac{P_u}{P} \Rightarrow P_u = F \cdot S \times P = 3.35 \times 36.667 = 122.83 \text{ kN}$$

$$\tau_u = \frac{P_{ult}}{A} = \frac{4 P_{ult}}{\pi d^2}$$

$$d = \sqrt{\frac{4 P_{ult}}{\pi \tau_{ult}}} = \sqrt{\frac{4 \times 122.83 \times 10^3}{\pi \times (360 \times 10^6)}} = 20.8 \text{ mm}$$



Stress on the rod ?
(type & Value)

Stress on the pin ?
(type & Value)

CORRECT ANSWER

Rod	$\sigma = 7.07 \text{ MPa}$	Pin	$\sigma = 0$
	$\tau = 0$		$\tau = 5.09 \text{ MPa}$

Rod 30 mm : —

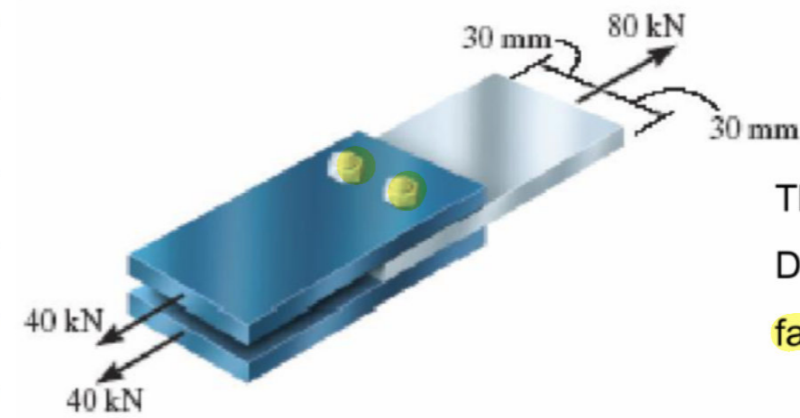
$$\sigma_{30 \text{ mm}} = \frac{P}{A} = \frac{5 \times 10^3}{\frac{\pi}{4} \left(\frac{30}{1000}\right)^2} = 7.1 \text{ MPa} \quad \left. \vphantom{\frac{P}{A}} \right\} \text{tensile stress}$$

Rod 40 mm : —

$$\sigma_{40 \text{ mm}} = \frac{5 \times 10^3}{\frac{\pi}{4} \left(\frac{40}{1000}\right)^2} = 3.98 \text{ MPa} \quad \left. \vphantom{\frac{5 \times 10^3}{\frac{\pi}{4} \left(\frac{40}{1000}\right)^2}} \right\} \text{tensile stress}$$

Double Shear @ Pin : —

$$\tau = \frac{P}{2A_{\text{pin}}} = \frac{5 \times 10^3}{2 \left(\frac{\pi}{4} \left(\frac{25}{1000}\right)^2\right)} = 5.1 \text{ MPa}$$



The joint is fastened together using two bolts. Determine the required diameter of the bolts if the failure shear stress for the bolts is $\tau_{\text{Fail}} = 350 \text{ MPa}$.

Use a factor of safety for shear of F.S. = 2.5.

$$\Rightarrow F.S. = \frac{\tau_{\text{ult}}}{\tau_{\text{av}}}$$

CORRECT ANSWER

$$d = 13.49 \text{ mm}$$

Shear is double

$$\tau_{\text{av}} = \frac{P}{2(2A)} = \frac{P}{4A}$$

$$\frac{\tau_{\text{ult}}}{F.S.} = \frac{P}{4A}$$

$$\frac{350 \times 10^6}{2.5} = \frac{80 \times 10^3}{4 \times \frac{\pi d^2}{4}}$$



$$d = 13.5 \text{ mm}$$

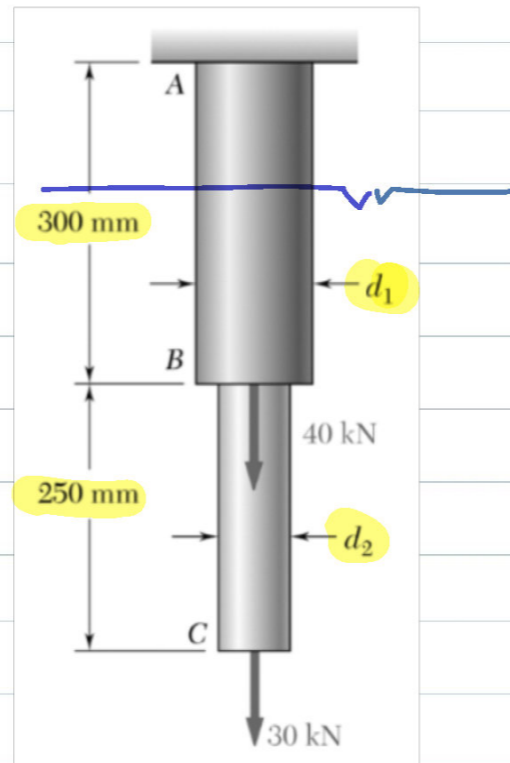
PROBLEM 1.2

Two solid cylindrical rods AB and BC are welded together at B and loaded as shown. Knowing that $d_1 = 50$ mm and $d_2 = 30$ mm, find the average normal stress at the midsection of (a) rod AB , (b) rod BC .

Rod AB : -

$$P_{AB} = 30 + 40 = 70 \text{ kN}$$

$$A_{AB} = \frac{\pi d_1^2}{4}$$
$$= \frac{\pi}{4} \left(\frac{50}{1000} \right)^2$$
$$= 1.9635 \times 10^{-3} \text{ m}^2$$



$$\sigma_{AB} = \frac{P_{AB}}{A} = \frac{70 \times 10^3}{1.9635 \times 10^{-3}} = 35.7 \times 10^6 \text{ Pa}$$
$$= 35.7 \text{ MPa}$$

Rod BC : -

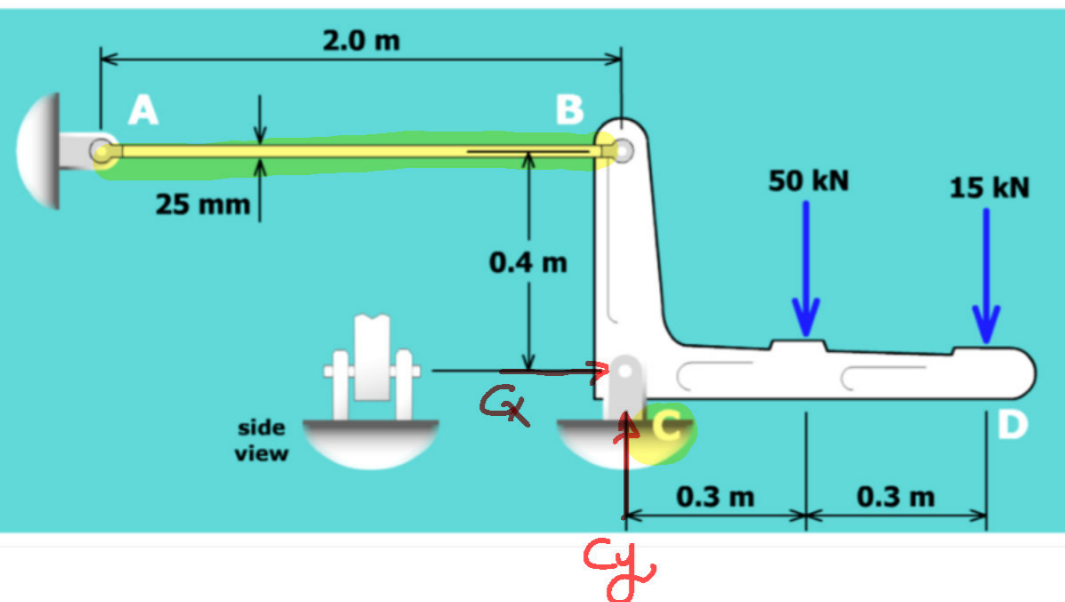
$$P_{BC} = 30 \text{ kN}$$

$$A_{BC} = \frac{\pi d_2^2}{4}$$

$$A_{BC} = \frac{\pi}{4} \left(\frac{30}{1000} \right)^2 = 706.86 \times 10^{-6} \text{ m}^2$$

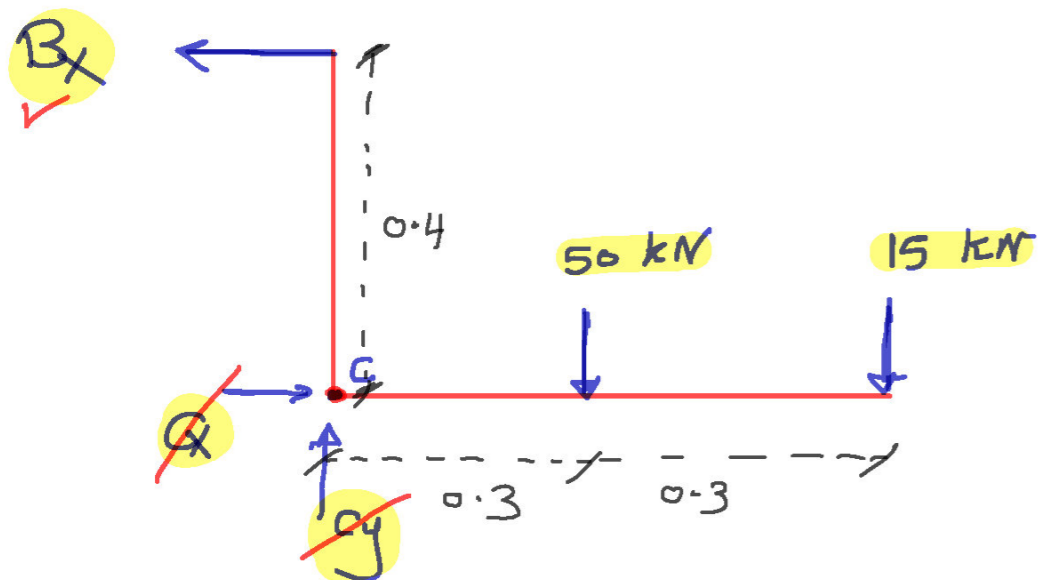
$$\sigma_{BC} = \frac{P}{A}$$

$$= \frac{30 \times 10^3}{706.86 \times 10^{-6}} = 42.4 \times 10^6 \text{ Pa}$$
$$= 42.4 \text{ MPa}$$



A pin C and a round aluminum rod at B support the rigid bar BCD. If the allowable shear stress for the pin is 50 MPa, what is the minimum diameter required for the pin at C?

$$\tau_{\text{all}} = 50 \text{ MPa}$$



$$\sum M_C = 0 \quad \uparrow +$$

$$B_x \times 0.4 - 50 \times 0.3 - 15 \times 0.6 = 0$$

$$B_x = 60 \text{ kN}$$

$$\sum F_x = 0 \quad \rightarrow +$$

$$C_x - 60 = 0 \Rightarrow C_x = 60 \text{ kN}$$

$$\sum F_y = 0 \quad \uparrow +$$

$$C_y - 50 - 15 = 0 \Rightarrow C_y = 65 \text{ kN}$$

$$F_C = \sqrt{C_x^2 + C_y^2}$$

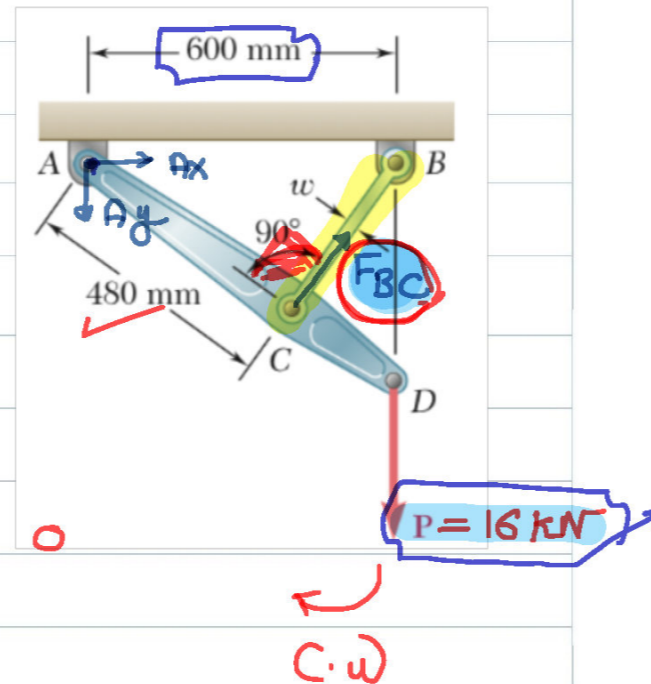
$$= \sqrt{(60)^2 + (65)^2} = 88.5 \text{ kN}$$

⇒ Double Shear @ Pin (C) : -

$$\tau_{\text{all}} = \frac{F_C}{2A} = \frac{F_C \times 4}{2\pi D^2}$$

$$D = \sqrt{\frac{2F_C}{\pi \tau_{\text{all}}}} = \sqrt{\frac{2 \times 88.5 \times 10^3}{\pi \times 50 \times 10^6}} = 33.6 \text{ mm}$$

1.37 Link BC is 6 mm thick, has a width $w = 25$ mm, and is made of a steel with a 480 -MPa ultimate strength in tension. What is the safety factor used if the structure shown was designed to support a 16 -kN load P ?



$$* \sigma_u = 480 \text{ MPa}$$

$$EM_A = 0 \quad \curvearrow +$$

$$F_{BC} \times 480 - 16 \times 600 = 0$$

$$F_{BC} = 20 \text{ kN}$$

$$* \sigma_u = \frac{F_{ult}}{A}$$

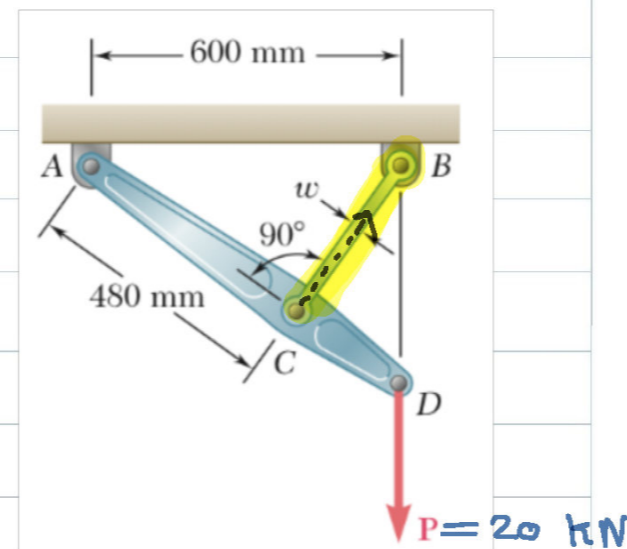
$$F_{ult} = \sigma_u \times A = 480 \times 10^6 \times 0.006 \times 0.025$$

$$= 72 \times 10^3 \text{ N}$$

$$* F.S. = \frac{F_{ult}}{F_{BC}} = \frac{72 \times 10^3}{20 \times 10^3}$$

$$= 3.6$$

1.38 Link **BC** is 6 mm thick and is made of a steel with a **450-MPa** ultimate strength in tension. What should be its width **w** if the structure shown is being designed to support a **20-kN** load **P** with a factor of safety of 3?



$$\sigma_{ult} = 450 \text{ MPa}$$

$$F \cdot S = 3$$

$$F \cdot S = \frac{\sigma_{ult}}{\sigma_{all}}$$

$$\sigma_{all} = \frac{\sigma_{ult}}{F \cdot S} = \frac{450}{3} = 150 \text{ MPa}$$

$$\sum M_A = 0 \quad \curvearrowright +$$

$$+ F_{BC} \cdot 480 - 20 \cdot 600 = 0$$

$$F_{BC} = 25 \text{ kN}$$

$$\text{Stress} = \frac{\text{Force}}{\text{Area}}$$

$$\sigma_{all} = \frac{F_{BC}}{A} \Rightarrow A = \frac{F_{BC}}{\sigma_{all}}$$

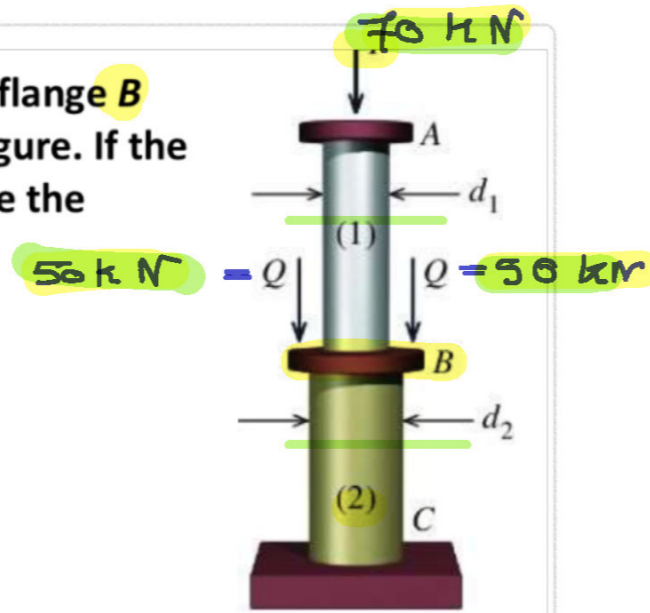
$$A = \frac{25 \times 10^3}{150 \times 10^6} = 1.67 \times 10^{-4} \text{ m}^2$$

$$A = w \cdot t$$

$$w = \frac{A}{t} = \frac{1.67 \times 10^{-4}}{0.006} = 0.0278 \text{ m}$$

$$w = 27.8 \text{ mm}$$

P1.3 Two solid cylindrical rods (1) and (2) are joined together at flange B and loaded with loads of $P = 70 \text{ kN}$ and $Q = 50 \text{ kN}$ as shown in Figure. If the normal stress in each rod must be limited to 210 MPa , determine the minimum diameter required for each rod.



Solution

$$\sigma = \frac{P}{A} = \frac{4P}{\pi d^2}$$

$$d = \sqrt{\frac{4P}{\pi \sigma}}$$

Rod (1)

$$P_{AB} = -70 \text{ kN}$$

$$\sigma_{AB} = -210 \text{ MPa}$$

$$d = \sqrt{\frac{4 \times -70 \times 10^3}{\pi \times -210 \times 10^6}}$$

$$= 20.6 \text{ mm}$$

Rod (2)

$$P_{BC} = -70 - 50 - 50 = -170 \text{ kN}$$

$$\sigma_{BC} = -210 \text{ MPa}$$

$$d = \sqrt{\frac{4 \times -170 \times 10^3}{\pi \times -210 \times 10^6}}$$

$$= 31.1 \text{ mm}$$